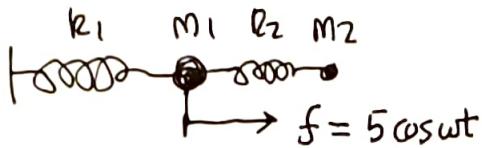


# EPC4 7.5.14 dynamic damping

①



$$k_1 = 50, k_2 = 10, m_1 = 1, \omega = 10$$

$$\begin{bmatrix} x_1 \\ x_2 \end{bmatrix}'' = \underbrace{\begin{bmatrix} -(k_1+k_2)/m_1 & k_2/m_1 \\ k_2/m_2 & -k_2/m_2 \end{bmatrix}}_{A} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} + \underbrace{\begin{bmatrix} 5 \cos \omega t \\ 0 \end{bmatrix}}_{F}$$

$$A = \begin{bmatrix} -60 & 10 \\ 10/m_2 & -10/m_2 \end{bmatrix}$$

Goal: Adjust  $m_2$  to make

the response displacement for  $x_1$ , zero. Use the method of undetermined coefficients for  $x_1, x_2$  to evaluate the particular soln, which is the response vector.

Trial soln:  $\mathbf{x} = \langle x_1, x_2 \rangle = \langle a \cos \omega t, b \cos \omega t \rangle$

$$x'' = -\omega^2 x = Ax + F$$

$$\cancel{(A + \omega^2 I)} x = F \rightarrow x = \cancel{(A + \omega^2 I)^{-1}} F$$

$$\det(A - (\omega^2 I)) \neq 0$$

$\neq$  eigenvalue of A

insert

coefficients of  $\cos \omega t$ :

Explicitly:

$$x_1'' + 60x_1 - 10x_2 = 5 \cos 10t \rightarrow -100a + 60a - 10b = 5$$

$$x_2'' - \frac{10}{m_2}x_1 + \frac{10}{m_2}x_2 = 0 \rightarrow -100b - \frac{10}{m_2}a + \frac{10}{m_2}b = 0$$

$$\underbrace{\begin{bmatrix} -40 & 10 \\ \frac{10}{m_2} & \frac{10}{m_2} - 100 \end{bmatrix}}_{\text{det} = 40(100 - \frac{10}{m_2}) - \frac{100}{m_2}} \begin{bmatrix} a \\ b \end{bmatrix} = \begin{bmatrix} 5 \\ 0 \end{bmatrix} \rightarrow \begin{bmatrix} a \\ b \end{bmatrix} = \frac{\begin{bmatrix} 10 - 100 \\ 10 \end{bmatrix} \begin{bmatrix} 5 \\ 0 \end{bmatrix}}{500(\frac{1}{m_2} - 1)} = \begin{bmatrix} 50(\frac{1}{m_2} - 1) \\ 50/m_2 \end{bmatrix}$$

$$\text{det} = 40(100 - \frac{10}{m_2}) - \frac{100}{m_2} = 500(\frac{1}{m_2} - 1)$$

If  $m_2 = \frac{1}{8}$ ,  $\det(A + \omega^2 I) = 0$  and  $\lambda = -100$  is an eigenvalue corresponding to eigenfrequency  $\omega = 10$ .

In this case the trial solution must be multiplied by t because the trial function is a homogeneous soln!

$$= \begin{bmatrix} \frac{1}{m_2} - 10 \\ \frac{1}{m_2} \end{bmatrix} \quad a = 0 : m_2 = 1/10 \\ \frac{1}{10(\frac{1}{8} - 1)} = -\frac{1}{2}$$

$$x = \langle 0, -\frac{1}{2} \cos 10t \rangle$$

↑ ↑

mass 1 is fixed, mass 2 oscillates in opposite direction to the force on mass 1 to compensate for the force on it from the second spring.

## EPC4 7.6.14 dynamic damping (2)

For  $m = 1/8$ :

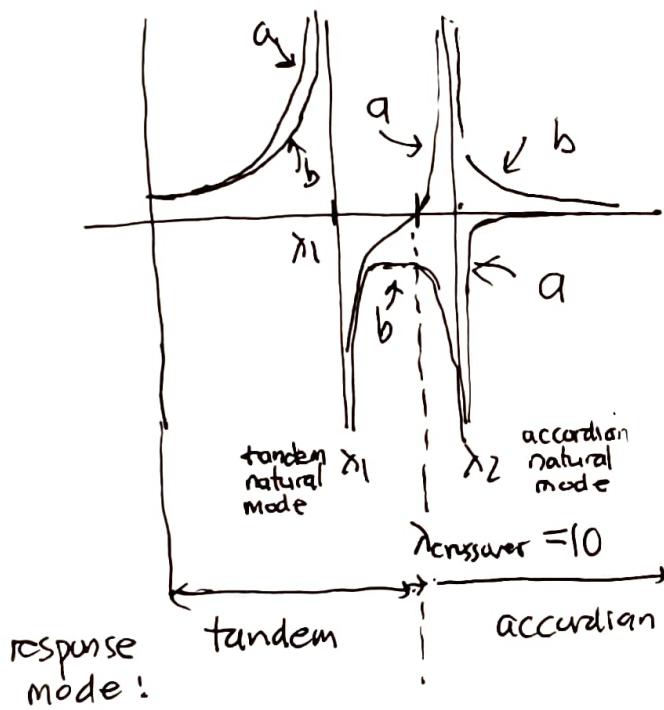
$$A = \begin{bmatrix} -60 & 10 \\ 100 & -100 \end{bmatrix} \quad B \approx \begin{bmatrix} 0.57 & -0.17 \\ 1 & 1 \end{bmatrix}$$

$$\lambda \approx 6.53 \quad 10.84$$

$\omega_1$   
tandem  
mode

$\omega_2$   
accordian  
mode

If we study the response coefficients  $[a(\omega), b(\omega)]$  for general frequency we find



$$\begin{bmatrix} x_1 \\ x_2 \end{bmatrix} = \begin{bmatrix} a(\omega) \cos \omega t \\ b(\omega) \cos \omega t \end{bmatrix}$$

$$f_1 = 5 \cos \omega t$$

↑  
just a convenient factor  
actual value unimportant.

It is the ratio of the applied force and the response amplitudes which matter.

This is typical for all of these 2 mass 2 spring systems.

The interval  $0 \leq \omega \leq \omega_{\text{crossover}}$  containing the tandem natural mode frequency has a tandem mode response same sign for  $a(\omega), b(\omega)$

for  $\omega > \omega_{\text{crossover}}$  containing the accordian mode frequency, the response mode is a accordian mode (opposite signs for  $a(\omega), b(\omega)$ )

The first mass is stationary at the crossover frequency, where the second spring contracts or stretches to balance the force applied directly to the first mass.

For fixed  $M_1, k_1$  one can always adjust the smaller mass-spring add-on to zero out the oscillations in the first mass.

# EPC4 7.6.14 dynamic damping (More!)

(3)

$$A = \begin{bmatrix} -\frac{(k_1+k_2)}{m_1} & \frac{k_2}{m_1} \\ \frac{k_2}{m_2} & -\frac{k_2}{m_2} \end{bmatrix} = \begin{bmatrix} -(w_1^2 + \gamma w_2^2) & w_2^2 \gamma \\ w_2^2 & -w_2^2 \end{bmatrix}$$

$$\omega_1^2 \equiv \frac{k_1}{m_1}$$

$$\omega_2^2 \equiv \frac{k_2}{m_2}$$

separate natural frequencies

$$\gamma = \frac{m_2}{m_1} \text{ mass ratio}$$

$$x = \begin{bmatrix} a \\ b \end{bmatrix} \cos \omega t, \quad x'' = -\omega^2 x$$

$$\downarrow \quad x'' - AX = \begin{bmatrix} w_1^2 + \gamma w_2^2 - \omega^2 & -\gamma w_2^2 \\ -\omega^2 & w_2^2 - \omega^2 \end{bmatrix} \begin{bmatrix} a \\ b \end{bmatrix} \cos \omega t = \begin{bmatrix} f_1 \cos \omega t \\ 0 \end{bmatrix}$$

$$\begin{bmatrix} w_1^2 + \gamma w_2^2 - \omega^2 & \gamma w_2^2 \\ -\omega^2 & w_2^2 - \omega^2 \end{bmatrix} \begin{bmatrix} a \\ b \end{bmatrix} = \begin{bmatrix} f_1 \\ 0 \end{bmatrix}$$

$$\begin{bmatrix} a \\ b \end{bmatrix} = \frac{1}{(w_1^2 + \gamma w_2^2 - \omega^2)(w_2^2 - \omega^2) + \gamma w_2^4} \begin{bmatrix} \gamma w_2^2 \\ w_1^2 w_2^2 - \omega^2 \end{bmatrix} \begin{bmatrix} f_1 \\ 0 \end{bmatrix} = \frac{f_1}{\gamma} \begin{bmatrix} w_2^2 - \omega^2 \\ w_2^2 \end{bmatrix}$$

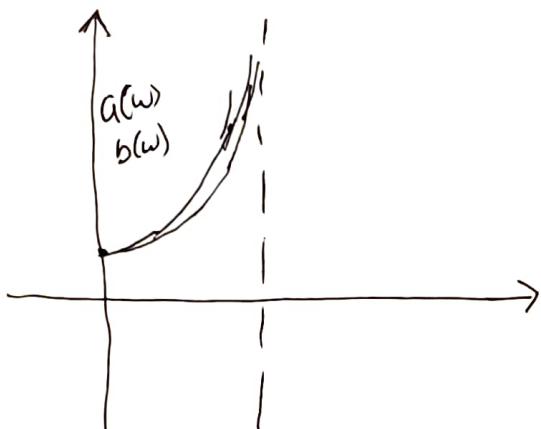
$$\text{if } a=0 \text{ means } \omega^2 = w_2^2, \quad \boxed{\omega = w_2}$$

The second mass natural frequency is used to drive the first mass or more precisely

The second mass was chosen to make the second mass spring natural frequency equal the driving frequency, which in turn is slightly less than the natural frequency of the combined system (accidental mode) where resonance occurs (when some damping is present).

Pushing this concrete problem with specific numbers to understand what lies behind it is the magic of mathematics.

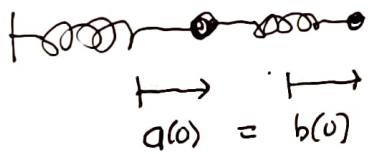
But we can actually understand some obvious features of the frequency response functions  $a(\omega), b(\omega)$ .



$\omega=0$  zero frequency limit

$\cos(\omega) = 1$ : constant force  
on first mass to right

both masses just move to  
new equilibrium equal distances  
to the right



since there is no third spring  
to compress the second spring

As  $\omega$  increases from zero  
to very small values, the system  
simply slowly moves to new  
equilibrium values moment by  
moment so remains in phase  
with the slowly changing  
driving force.