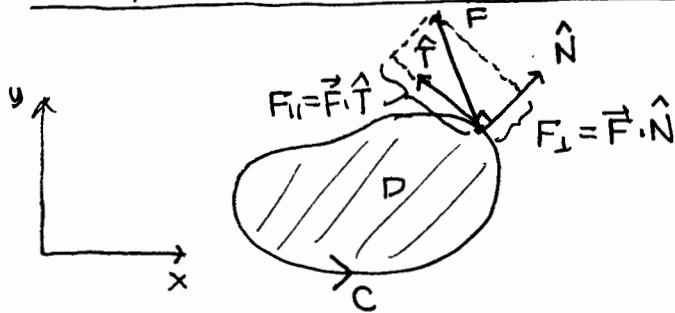


## interpretation of divergence and curl (2d)



C: counter clockwise loop with interior D

T-hat: unit counterclockwise tangent

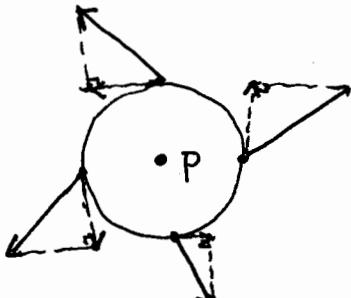
N-hat: unit outer normal

$F_{\parallel} = \vec{F} \cdot \hat{T}$  tangential component along curve

$F_{\perp} = \vec{F} \cdot \hat{N}$  normal component along curve

### Green-Stokes

$$\oint_C \vec{F} \cdot \hat{T} ds = \text{circulation of } \vec{F} \text{ (counterclockwise) around } C = \iint_D \text{curl}(\vec{F})_z dA$$



To interpret the value of  $\text{curl}(\vec{F})_z$  at a point P, shrink a small loop (circle or rectangle) down around P until the value of  $\text{curl}(\vec{F})_z$  across the loop is almost constant (within some tolerance).

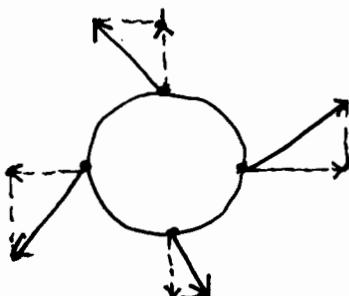
only  $F_{\parallel}$  contributes to the circulation around a loop

$$\approx \text{curl}(\vec{F})_z|_P \cdot \text{area}(D)$$

if nonzero there must always be a net circulation around the loop proportional to the area of the loop, in the counterclockwise sense if positive, clockwise if negative.

### Green-Gauss

$$\oint_C \vec{F} \cdot \hat{N} ds = \text{net flux of } \vec{F} \text{ out of loop } C = \iint_D \text{div}(\vec{F}) dA$$



Again shrink a loop down around P until the value of  $\text{div}(\vec{F})$  is almost constant across the loop

only  $F_{\perp}$  contributes to the flux in or out of the loop

$$\approx \text{div}(\vec{F})|_P \cdot \text{area}(D)$$

if nonzero there must always be a net flux in (if negative) or out (if positive) of the loop

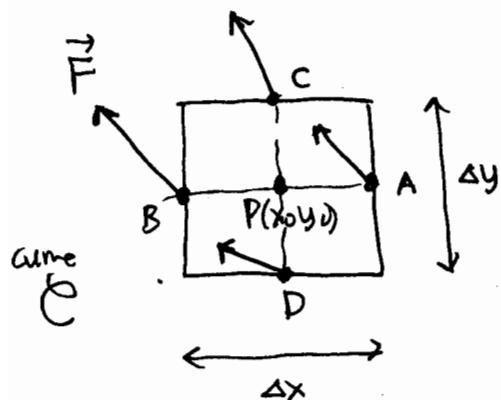
## interpretation of divergence and curl (2d) continued

### WARNING! PROCEED AT YOUR OWN RISK. OPTIONAL MATERIAL

When one first sees these things in physics for the first time a student has no clue how to evaluate a line or flux integral except if the tangential or normal component is a constant and the curve is a circle so calculus is unnecessary (!).

Starting from this lack of knowledge one can then derive component formulas for the divergence and curl from a limiting ratio.

Here we examine  $\text{curl}(\vec{F})_z$  and the circulation, using a rectangular curve  $C$  of width  $\Delta x$  and height  $\Delta y$ . We approximate  $\vec{F}$  by pretending it is constant on each side of the box using its midpoint value for the approximate constant value & evaluate those 4 values using Taylor series centered at  $P$ .



counterclockwise tangential components:

- side A :  $F_y(A)$  length  $\Delta y$
- side B :  $-F_y(B)$  length  $\Delta y$
- side C :  $-F_x(C)$  length  $\Delta x$
- side D :  $F_x(D)$  length  $\Delta x$

(physics vector notation:  
 $\vec{F} = \langle F_x, F_y, F_z \rangle$ )

$$\oint_C \vec{F} \cdot \hat{T} ds \approx \underbrace{\left[ F_y(x_0, y_0) + \frac{\partial F_y}{\partial x}(x_0, y_0) \left( \frac{\Delta x}{2} \right) \right] \Delta y}_{\text{value at midpt A}} - \underbrace{\left[ F_x(x_0, y_0) + \frac{\partial F_x}{\partial y}(x_0, y_0) \left( \frac{\Delta y}{2} \right) \right] \Delta x}_{\text{value at midpt C}}$$

$$- \underbrace{\left[ F_y(x_0, y_0) + \frac{\partial F_y}{\partial x}(x_0, y_0) \left( -\frac{\Delta x}{2} \right) \right] \Delta y}_{\text{value at midpt B}} + \underbrace{\left[ F_x(x_0, y_0) + \frac{\partial F_x}{\partial y}(x_0, y_0) \left( -\frac{\Delta y}{2} \right) \right] \Delta x}_{\text{value at midpt D}}$$


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$$\text{sum: } = 0 + \frac{\partial F_y}{\partial x}(x_0, y_0) \Delta x \Delta y + 0 - \frac{\partial F_x}{\partial y}(x_0, y_0) \Delta x \Delta y$$

$$= \left( \frac{\partial F_y}{\partial x} - \frac{\partial F_x}{\partial y} \right)(x_0, y_0) \Delta x \Delta y$$

In the limit  $C$  shrinks to  $P$  we obtain

$$\text{curl}(\vec{F})_z = \lim_{C \rightarrow P} \frac{\oint_C \vec{F} \cdot \hat{T} ds}{\text{area}(C)} = \frac{\partial F_y}{\partial x} - \frac{\partial F_x}{\partial y}$$

a similar calculation for the outward flux integral produces

$$\text{div}(\vec{F}) = \lim_{C \rightarrow P} \frac{\oint_C \vec{F} \cdot \hat{N} ds}{\text{area}(C)} = \frac{\partial F_x}{\partial x} + \frac{\partial F_y}{\partial y}$$